

550.36-504.3

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Chemical processes that flow in rocks under the influence of hot water and high temperature during exploitation industrial furnaces and application of basic conformities to the law of chemical thermodynamics are considered. Equalizations that describe changes in thermodynamics descriptions of rocks are given.

Key words: rocks, hot water, temperature, thermal behavior, ecological balance.

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 2000 , 7 10- ;
 () 9 10- ;
 120...170 , —
 6...6,5). (,
 — 3,5...5,5),
 , (,),
 , .

(G). (C_p)

$$C_p = a + bT + cT^{-2}, \quad (1)$$

a, b, c – ; T –

$$a = 11,67, b = 1,08 \cdot 10^3, c = -1,56 \cdot 10^{-5};$$

$$a = 22,64, b = 3,6 \cdot 10^3, c = -6,52 \cdot 10^{-5};$$

$$a = 11,22, b = 8,2 \cdot 10^3, c = -2,7 \cdot 10^{-5};$$

$$a = 8,85, b = 0,16 \cdot 10^3, c = -0,68 \cdot 10^{-5};$$

$$\text{Fe}_2\text{O}_3 \quad a = 23,49, b = 18,6 \cdot 10^3, c = -3,55 \cdot 10^{-5}$$

25...800 ° .

(, , , . .),

$$S_2 - S_1 = \Delta S = \int_{T_1}^{T_2} \frac{C_p}{T} dT. \quad (2)$$

$$H = U + PV, \quad (3)$$

U V – ; P – .

$$H_2 - H_1 = \Delta H = \int_{T_1}^{T_2} C_p dT. \quad (4)$$

$$G = U - TS + PV = H - TS, \quad (5)$$

(5)

$$dG = -SdT - VdP \quad (6)$$

:

$$G_2 - G_1 = \Delta G = - \int_{T_1}^{T_2} S dT + \int_{P_1}^{P_2} V dP. \quad (7)$$

[1-7]

298,15 (25 °)

1

1. CaO - $M = 56,079$;
 $\Delta H = -16,764$ / ; $\Delta S = -152796$ /
 (25 °); $S = 9,5$
2. CaSiO₃ - $M = 116,164$; $M_o = 39,93$ ³ ;
 $\Delta H = -389070$ ° ; $S = 20,9$
3. Fe₂O₃ - $M = 159,692$; $M_o = 30,274$ ³ ;
 $\Delta H = -197100$ ° ; $S = 20,89$
4. MgO - $M = 40,311$; $M_o = 11,248$ ³ ;
 $\Delta H = -143500$ ° ; $S = 6,34$
5. MgSiO₃ - $M = 396$; $M_o = 31,47$ ³ ;
 $\Delta H = -370143$ ° ; $S = 16,30$
6. SiO₂ - $M = 60,085$; $M_o = 22,688$ ³ ;
 $\Delta H = -216902$ ° ; $S = 10,43$
7. FeSiO₃ - $M = 131,932$; $M_o = 33,52$ ³ ;
 $\Delta H = -285700$ ° ; $S = 22,18$, 1 = 4,1858

$$S \quad (2).$$

$$S = \int_0^T \frac{C_p}{T} dT. \quad (8)$$

$$\Delta G = H - T\Delta S, \tag{9}$$

G

$$\Delta G_{25^\circ C}^\alpha = \Delta H_{25^\circ C}^\alpha - 25^\circ C \cdot \Delta S_{25^\circ C}^\alpha, \tag{10}$$

$\Delta S_{25^\circ C}^\alpha -$

S

; $\Delta H_{25^\circ C}^\alpha -$

H

25 °C.

$\alpha \quad \alpha$

ΔH

ΔS

$\alpha-$

ΔG

($dP = 0$)

$$G_2 - G_1 = \Delta G = - \int_{T_1}^{T_2} SdT. \tag{10'}$$

SiO₂ –

$\beta-$

26,5 / ³ –

575 °

$\alpha-$

870 °

22,6 / ³,

1470 °

$\beta-$

1710 °

23 / ³.

25 °

$\Delta G_{25^\circ C}^\alpha = -204646$ /

;

25 ° 870 °

$\beta-$

$\Delta G_{870^\circ C}^{\beta-Q} = -222630$ /

;

$\Delta G_{1470^\circ C}^{\beta-Tr} = -222702$

/ ;

$\beta-$

$\Delta G_{>1470^\circ C}^{\beta-Cr} = -243248$

(0,07 1),

() 10 %-

« »

CO₂



CO_2 ,

$\text{Ca}(\text{HCO}_3)_2$,

100, CaCO_3 .

S , H , C_p ,

γ 750 °, C_p

(1) : $a = 3,04, b = 7,58 \cdot 10^3, c = 0,6 \cdot 10^{-5}$,

750 ° C_p

$a = 6,74, b = 7,60 \cdot 10^3, c = 0,63 \cdot 10^{-5}$.

$$S_T = S_{25^\circ C}^\alpha + \int_{25^\circ C}^{T_1} \frac{C_p'}{T} dT + \Delta S_{T_1}^{nep} + \int_{T_1}^{T_2} \frac{C_p''}{T} dT + \Delta S_{T_2}^{nep} + \dots + \Delta H \int_{T_{n-1}}^{T_n} \frac{C_p^n}{T} dT + \Delta S_{T_{n-1}}^{nep}, \quad (11)$$

T_1, T_2, T_{n-1} ; $\Delta S_{T_1}^{nep}, \Delta S_{T_2}^{nep}, \dots, \Delta S_{T_{n-1}}^{nep}$ – 1- , 2- , ..., (n-1)-
 ; $C_p', C_p'', \dots, C_p^n$ – 1- , 2- , ... , n-
 C_p (1)
 (11)

$$S_T^\alpha = S_{25^\circ C}^\alpha + \alpha' A_s' + b' B_s' + c' C_s' + \Delta S_{T_1}^{\alpha'} + \alpha'' A_s'' + b'' B_s'' + c'' C_s'' + \Delta S_{T_2}^{\alpha''} + \dots + a^n A_s^n + b^n B_s^n + c^n C_s^n + \Delta S_{T_{n-1}}^{\alpha^n} \quad (12)$$

$$A_s' = \ln \frac{T_1}{25^\circ C}; B_s' = (T_1 - 25^\circ C); C_s' = \frac{1}{2} \left(\frac{1}{25^\circ C^2} - \frac{1}{T_1^2} \right);$$

$$A_s'' = \ln \frac{T_2}{T_1}; B_s'' = (T_2 - T_1); C_s'' = \frac{1}{2} \left(\frac{1}{T_2^2} - \frac{1}{T_1^2} \right);$$

.....
 $A_s^n = \ln \frac{T_n}{T_{n-1}}; B_s^n = (T_n - T_{n-1}); C_s^n = \frac{1}{2} \left(\frac{1}{T_n^2} - \frac{1}{T_{n-1}^2} \right);$

$a', b', c', a'', b'', c'', \dots, a^n, b^n, c^n$ – C_p

$$\Delta G_T^{nep} = 0$$

$$\Delta S_T^{nep}$$

$$\Delta S_T^{ep} = \frac{\Delta H_T^{ep}}{T^{ep}}. \tag{13}$$

$$(12)$$

:

$$\Delta H_T^\alpha = \Delta H_{25^\circ C} + \int_{25^\circ C}^{T_1} C_p' dT + \Delta H_{T_1} + \int_{25^\circ C}^{T_2} C_p dT + \Delta H_{T_2} + \dots + \int_{T_{n-1}}^{T_n} C_p^n dT + \Delta H_{T_{n-1}}, \tag{14}$$

$$\Delta H_{T_1}^{ep}, \Delta H_{T_2}^{ep}, \dots, \Delta H_{T_{n-1}}^{ep} - 1-, 2-, \dots, (n-1)-$$

$$\Delta H_T = \Delta H_{25^\circ C}^\alpha + a'A_H' + b'B_H' + c'C_H' + \Delta H_{T_1}^{nep} + a''A_H'' + b''B_H'' + c''C_H'' + \Delta H_{T_2}^{nep} + \dots + a^n A_H^n + b^n B_H^n + c^n C_H^n + \Delta H_{T_{n-1}}^{nep}, \tag{15}$$

$$A_H' = (T_1 - 25^\circ C); B_H' = \frac{1}{2}(T_1^2 - 25^\circ C); C_H' = \frac{1}{25^\circ C} - \frac{1}{T_1};$$

$$A_H'' = (T_2 - T_1); B_H'' = \frac{1}{2}(T_2^2 - T_1^2); C_H'' = \frac{1}{T_1} - \frac{1}{T_2};$$

$$\dots\dots\dots A_H^n = (T_n - T_{n-1}); B_H^n = \frac{1}{2}(T_n^2 - T_{n-1}^2); C_H^n = \frac{1}{T_n} - \frac{1}{T_{n-1}}.$$

$$S_T \quad \Delta H_T$$

:

$$\Delta G_T = \Delta H_T - TS_T^\alpha. \tag{16}$$

$$\Delta S \quad T,$$

$T = \text{const},$

$$\Delta S = - \left(\frac{\partial V}{\partial T} \right)_P dP, \tag{17}$$

(V)

:

$$v = \frac{1}{V_0} \left(\frac{\partial V}{\partial T} \right)_P, \tag{18}$$

$V_0 -$

$T = 25^\circ C.$

$$(dT = 0)$$

$$(G_p - G_{P=1}) T^\alpha = \int_1^P V dP, \quad (19)$$

$$\Delta H_T, \quad dT \neq 0, \quad S_T \quad (16)$$

1.

2.

3.

4.

527

1.

2.

3.

4.

1. . . , .: , 1963. -
 2. . . . - .: . - 1968. - 520 .
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